Noncircular gears Theory and applications

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GIF source: http://www.gearandrack.com/non\_circular\_gears/simulation\_test\_for\_non\_circular\_gears.html



#### Introduction

- Noncircular gears (NCGs) first sketched by Leonardo da Vinci (1500)
- First known publications came in the 19th century
- A comprehensive overview of the non-circular gears was done by Litvin
- Limited data available especially compared to cylindrical gears



Picture source: H.T. Brown, Five Hundred and Seven Mechanical Movements

Picture source: B. Laczik, Design and Manufacturing of Non-Circular Gears by Given Transfer Function



35

mm



#### Introduction

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#### **Advantages**

- Variable transmission ratio
- Variable speed and torque
- Variable center distance
- Manufacturing process (if plastic or sinter)

#### Limitations

- Vibrations if not rotating in mass centre
- Strength calculation
- Manufacturing process (if steel)



Picture source: www.machinedesign.com/motorsdrives/noncircular-gears-make-unconventional-moves



• Cylindrical gears: operating pitch lines are circles

• Non-circular gears: operating pitch lines are NOT circles

According to the law of gear meshing, the operating pitch lines must roll together without slip!

Picture source: www.machinedesign.com/motorsdrives/noncircular-gears-make-unconventional-moves





- The **operating pitch lines** can be described by  $r_1(\phi_1)$  and  $r_2(\phi_2)$ .
- The transmission ratio function can be written as

$$i(\varphi_1) = \frac{\omega_1(\varphi_1)}{\omega_2(\varphi_2)} = \frac{r_2(\varphi_2)}{r_1(\varphi_1)}$$
 (eq. 1)

• The **center distance** is defined as

$$r_1(\varphi_1) + r_2(\varphi_2) = a = const$$
 (eq. 2)

• Eq. 1 can be rewritten to

$$i(\varphi_1) = \frac{a - r_1(\varphi_1)}{r_1(\varphi_1)}$$
 (eq. 3)





• Law of gearing: operating pitch lines must roll without slip  $r_1(\varphi_1)d\varphi_1 = r_2(\varphi_2)d\varphi_2$ 

$$d \varphi_2 = rac{r_1(\varphi_1)}{r_2(\varphi_2)} d \varphi_1$$
 (eq. 4)

• Calculation case 1:  $r_1(\phi_1)$  is known

$$d\varphi_2 = \frac{r_1(\varphi_1)}{a - r_1(\varphi_1)} \ d\varphi_1$$

$$\varphi_2 = \int_0^{\varphi_1} \frac{r_1(\varphi_1)}{a - r_1(\varphi_1)} \, d\varphi_1$$





• Law of gearing: operating pitch lines must roll without slip  $r_1(\varphi_1)d\varphi_1 = r_2(\varphi_2)d\varphi_2$ 

$$d\varphi_{2} = \frac{r_{1}(\varphi_{1})}{r_{2}(\varphi_{2})}d\varphi_{1} = \frac{1}{i(\varphi_{1})}d\varphi_{1}$$

• **Calculation case 2**:  $i(\varphi_1)$  is known

$$d\varphi_2 = \frac{1}{i(\varphi_1)} \, d\varphi_1$$

$$\varphi_2 = \int_0^{\varphi_1} \frac{1}{i(\varphi_1)} \, d\varphi_1$$





 To have continuous rotation of the non-circular gears, the operating pitch lines must be closed centrodes





Where  $n_1$  and  $n_2$  are Z<sup>+</sup>.







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 In case of unclosed centrodes, the angular rotation (or lateral movement) of the engaging gears is limited





- Curves used for operating pitch lines
  - Ellipses
  - N-lobbed ellipses
  - Circles with eccentricity
  - Arbitrary curves
- Additional eccentricity
- Variable center distance









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#### Variation of center distance



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# Rack and pinion design



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#### Generation of tooth form

The tooth form of the noncircular gears can be generated by a reference rack. In order to generate the tooth form, the reference lines must roll without slip. To produce the inner noncircular gears, a pinion type cutter must be used. A pinion type cutter can also be used to produce outer gears.

When using sintered or plastic material, then hobbing cutters or pinion type cutters are not required.

- No standardized strength calculation is available for noncircular gears
- Noncircular gear can be momentarily represented as a cylindrical gear
- Calculation with replacement cylindrical gear can be used
- Identification of critical teeth
  - Most loaded tooth
  - Tooth with the highest undercut
  - Ratio load/root thickness
  - Smallest root radius
  - ....





- Creating cylindrical replacement gear
- Operating pitch diameters from 'local' curvatures







- Normal module and pressure angle from noncircular gears
- Tip/root diameters for both gears
- Centre distance





- Tangential force and rotational speed have to be recalculated based on the new center points O<sub>1</sub> and O<sub>2</sub>
- Strength calculation is then performed using ISO 6336 or VDI 2736





# Noncircular gears in KISSsoft

The operating pitch lines are currently calculated in an Excel (and imported in KISSsoft)

			-		 		~		-	
NCG elliptical pitch line gear calculation (G1-G2)				SET eccentricity			Calua DK Calu			
		k (intiger)	PK	EK	focal point = 1		Solve CD	Solve PR	Solve LK	
Scale geometry	Ellipse with:	1	8.000000	0.500000	center point = 2					
ocale geometry					user input = 3					
Scale factor	10				Offset [mm]					
Ratio	1							Calculate n	nodule G1	
Speed Gear 1 [rpm]	1		Operating pitch I	ine length (mm)				z	25	
Center distance CD [m	m] 21.333		G1	62.61171	MAX ratio	MIN ratio		mn	0.797197	
Start angle [°]	0		G2	62.61171	3.0000	0.3333				
End angle [°]	360									
Angle increment [°]	0.1		Rotation a	angle (°)				Calculate number of teet		
tproU= (sec)	60		G1	360.0000	SOLVER			mn	0.797197	
First cell	18		G2	360.0000	5.8253E-20			z1	25.000	
Last cell	3618							z2	25.000	

- The operating pitch lines are defined in polar coordinates or as a \*.dxf file
- The operating pitch lines must be prolonged at the beginning and end for at least 30°







#### Noncircular gears in KISSsoft

Several different options available in KISSsoft

NG NG	Type of center distance	fixed			Type of center distance
Input: OPERATI PITCH LI	Generate Specification Operating pitch line gear 1	a Oper ellips	rating pitch line	/ mm / / ]	Generate Specification Operating pitch line gear 1 Operating pitch line gear 2
ıt: ISSION IO	Type of center distance Center distance	fixed	~ 30.0000000	mm	Type of center distance Generate
Inpu RANSMI RATI	Generate Specification Ratio	Ratio	<b>)</b>		Specification Ratio Operating pitch line gear 1
Ē					

#### **Center distance: FIXED**

#### **Center distance: VARIABLE**

Operating pitch line

variable

Input...

Type of center distance	variable	~
Generate		
Specification	Ratio	~
Ratio	Input	
Operating pitch line gear 1	ellipse_G1.DAT	



# Noncircular gears in KISSsoft – Tab Basic data

Basic data 🗗 Reference	orofile 🗗 🛛 Tolerances 🗗							
Geometry								
Normal module m	n	1.07763900	mm			Gear 1	Gear 2	
Normal pressure angle a <sub>r</sub>		18.00000000	o	Number of teeth	z	25	25	
Pinion type cutter 1	spur gear	~		Facewidth	b	1.00000000	1.00000000	mm
Helix angle of pinion type cutter $\beta_0$		0.00000000	0	Tip rounding	r	0.3000000	0.3000000	mm
Type of center distance	fixed	~						
Center distance a		30.00000000	mm					
Generate								
Specification	Ratio	~		Position of starting angle Gear 1		Middle root	~	
Ratio	Input			Starting angle	φa	0.00000000	180.00000000	0
				End angle	Φe	360.0000000	-180.00000516	0



# Noncircular gears in KISSsoft – Tab Reference profile

Basic data 📑 Reference profile	Tolerances				
Final machining Gear 1		Final machining Gear 2			
Tool selection	Cutter/Tool: Pinion type cutter	Tool selection		Cutter/Tool: Pinion type cutter	i
Designation	Own Input	Designation		Own Input	
Number of teeth z <sub>0</sub>	20	Number of teeth	Z <sub>0</sub>	20	
Profile shift coefficient x <sub>0</sub>	0.0000000	Profile shift coefficient	X <sub>0</sub>	0.0000000	
Addendum coefficient h <sup>*</sup> <sub>aP0</sub>	1.45000000	Addendum coefficient	$h^*_{aP0}$	1.45000000	
Tip form	Rounding	Tip form		Rounding ~	
Tip radius coefficient $\rho^*_{aP0}$	0.05000000	Tip radius coefficient	$\rho^*_{aP0}$	0.05000000	
$\label{eq:definition} \text{Dedendum coefficient} \qquad  \textbf{h}^*_{\text{fPO}}$	1.0000000	Dedendum coefficient	$h_{\rm fP0}^{*}$	1.0000000	
Root radius coefficient $\rho^*_{fP0}$	0.05000000	Root radius coefficient	$\rho^*_{fP0}$	0.05000000	
Protuberance height coefficient $h_{prP0}^{*}$	0.0000000	Protuberance height coefficient	$h^*_{prP0}$	0.0000000	
Protuberance angle aprP0	0.00000000 °	Protuberance angle	a <sub>prP0</sub>	0.0000000	0
Root form height coefficient $h_{FP0}^*$	0.0000000	Root form height coefficient	$h_{\rm FfP0}^{*}$	0.0000000	
Profile angle of the chamfer flank $\alpha_{\!K\!P\!0}$	0.00000000 °	Profile angle of the chamfer flank	( a <sub>KP0</sub>	0.0000000	0
✓ Topping tool		✓ Topping tool			



#### Noncircular gears in KISSsoft – Tab Reference profile

Basic data 🛛 🗗	Reference profile 🗗	Tolerances	ð					
Tolerance field								
Tolerance field for to	Tolerance field for tooth form display Mean value ~							
Allowances								
Gear 1 Gear 2								
Tooth thickness allow	vance (upper/lower) A <sub>sn</sub>	-0.120000	00	-0.32000000	mm	A <sub>sn</sub>	-0.12000000	-0.32000000 mm

Module specific settings

K Module specific settings		?	×
Approximation for export	t		
Curve type	Splines	~	
Permissible deviation $\boldsymbol{\epsilon}$		0.00000000	μm
		OK Ca	ncel



# Noncircular gears in KISSsoft – Tooth form examples



# Noncircular pinion and rack





#### Case study 1

- Cylindrical gears with constant transmission ratio i = 10
- Implementation of the non-circular gear stage
  - Reducing the motor size to half
  - Implementation of the stop positions in the design







#### Case study 2

• 3 non-circular gear train with transmission ratio  $i = 1 \pm 0.25$ 



1st and 3rd gears are cylindrical gears with an offset of 0.65 mm







#### Case study 3

- Cable braided sleeving machines
- Gears with revolutions 1:1
- Variation of transmission ratio: 1:6







# Module Z40

- Currently the KISSsoft module is sold together with a 1-time engineering
- The customer gets the Excel file to generate the operating pitch lines and instructions on how to generate the tooth form in KISSsoft
- He can then modify the Excel and use it for his next projects



# Thank you for your attention!

Sharing Knowledge

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